

Control of industrial robots

(Prof. Rocco)

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Name:

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Warnings:

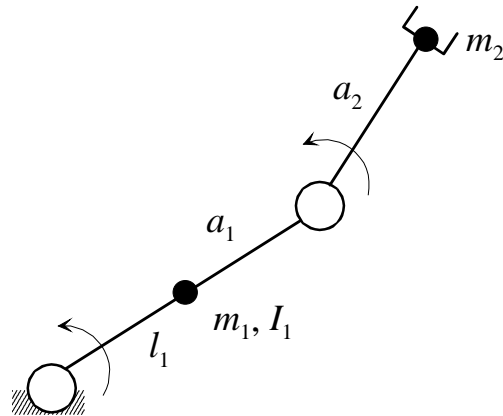
- This file consists of **8** pages (including cover). All the pages should be signed.
- During the exam you are not allowed to exit the room for any other reason than handing your work or withdrawing from the exam.
- You are not allowed to withdraw from the exam during the first 30 minutes.
- During the exam you are not allowed to consult books or any kind of notes.
- You are not allowed to use calculators with graphic display.
- Solutions and answers can be given **either in English or in Italian**.
- Solutions and answers must be given **exclusively in the reserved space**. Only in the case of corrections, or if the space is not sufficient, use the back of the front cover.
- The clarity and the order of the answers will be considered in the evaluation.
- At the end of the test you have to **hand this file only**. Every other sheet you may hand will not be taken into consideration.

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Use this page ONLY in case of corrections or if the space reserved for some answers turned out to be insufficient

Exercise 1

Consider the planar manipulator in the vertical plane sketched in the picture, where the mass of the second link is assumed to be concentrated at the end-effector



1.1 Find the expression of the inertia matrix of the manipulator.

1.2 Find the expression of the gravitational torques for this specific manipulator

1.3 Assume now $m_1 = 50$ Kg, $m_2 = 20$ Kg, $I_1 = 10$ Kg m², $a_1 = a_2 = 1$ m, $l_1 = 0.5$ m.

Suppose that you want to use the expression of the inertia matrix computed in section 1.1 to tune a decentralized position/velocity controller. Find suitable values for the moments of inertia on the load side (J_{l1} , J_{l2}) for the design of the controllers for joints 1 and 2.

1.4 Assume now that the joints of the robot are affected by elasticity. Find the values of the stiffness constants K_{el1} , K_{el2} , such that, taking as values of the reduction ratios $n_1 = n_2 = 100$, the locked frequencies for both the joints are 100 rad/s.

Exercise 2

- 2.1** Explain what is meant with kinematic scaling of a trajectory and write the general expression of a trajectory in the form (parameterized) which is used in such scaling.

- 2.2** The parametric form of a cycloidal trajectory is given by:

$$\sigma(\tau) = \tau - \frac{1}{2\pi} \sin(2\pi\tau)$$

Find the expressions of the maximum velocity and maximum acceleration for such trajectory in terms of the positioning time T and the total displacement h .

- 2.3** Consider the design of a cycloidal trajectory from $q_i = 10$ to $q_f = 40$, with $\dot{q}_{\max} = 30$, $\ddot{q}_{\max} = 10$. Find the minimum positioning time.

- 2.4** Suppose now that for the same problem of the previous question, a harmonic trajectory is used. Do you expect a longer or a shorter minimum positioning time? Explain your answer.

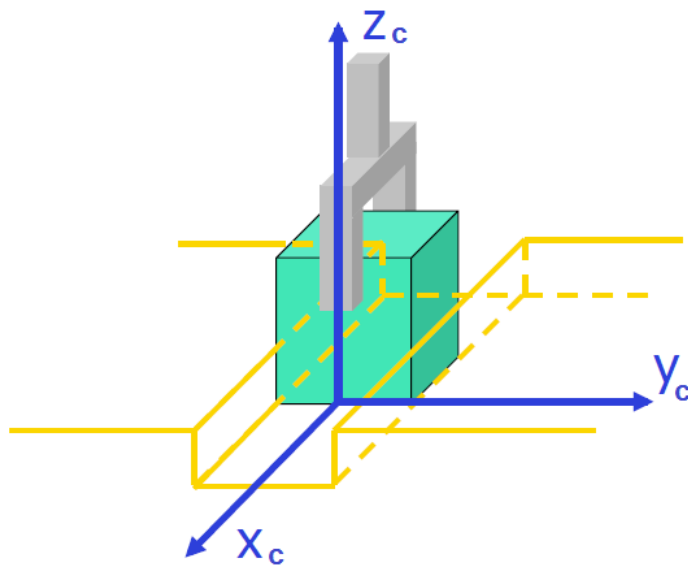
Exercise 3

- 3.1** Write the expression of a “PD plus gravity compensation” control law in joint space.
- 3.2** Write the expression of the “PD plus gravity compensation” control law in the operational space and sketch the related block diagram
- 3.3** Write the expression of the Lyapunov function used to prove the stability property of such control scheme, both for the joint space controller and for the operational space controller.

- 3.4** The stability proof for this control scheme is based on a property of the dynamic model of the robot manipulator. Specify what is this property.

Exercise 4

Consider an interaction task of a manipulator (sliding a cube along a guide), with a frictionless and rigid surface, as in this picture:



- 4.1** Based on the contact frame shown in the picture, express the natural and the artificial constraints for this problem.

- 4.2** Write the expression of the selection matrix for this problem, explaining the meaning of such matrix.
- 4.3** Suppose now that along the z direction an explicit force controller has to be designed. Find the expression of such controller, taking a bandwidth of 20 rad/s.
- 4.4** Sketch the block diagram of the controller of the previous question, when it is designed as an implicit force controller. What is the advantage in using an implicit controller?